# **Gear Geometry and Applied Theory**

## SECOND EDITION

Faydor L. Litvin

University of Illinois at Chicago

## **Alfonso Fuentes**

Polytechnic University of Cartagena



## PUBLISHED BY THE PRESS SYNDICATE OF THE UNIVERSITY OF CAMBRIDGE The Pitt Building, Trumpington Street, Cambridge, United Kingdom

#### CAMBRIDGE UNIVERSITY PRESS

The Edinburgh Building, Cambridge CB2 2RU, UK 40 West 20th Street, New York, NY 10011-4211, USA 477 Williamstown Road, Port Melbourne, VIC 3207, Australia Ruiz de Alarcón 13, 28014 Madrid, Spain Dock House, The Waterfront, Cape Town 8001, South Africa

http://www.cambridge.org

© Faydor L. Litvin and Alfonso Fuentes 2004

This book is in copyright. Subject to statutory exception and to the provisions of relevant collective licensing agreements, no reproduction of any part may take place without the written permission of Cambridge University Press.

First published 2004

Printed in the United States of America

Typefaces Sabon 10/13 pt. and Gill Sans System LATEX  $2_{\varepsilon}$  [TB]

A catalog record for this book is available from the British Library.

Library of Congress Cataloging in Publication Data

Litvin, F. L. (Faydor L.)

Gear geometry and applied theory / Faydor L. Litvin, Alfonso Fuentes.

o. cm.

Includes bibliographical references and index.

ISBN 0-521-81517-7

1. Gearing. I. Fuentes, Alfonso. II. Title

TJ184.L48 2004

621.8'33 - dc22

2003065205

ISBN 0 521 81517 7 hardback

Foreword by Graziano Curti		page xii
Pre	face	xiv
Ack	nowledgments	xv
ı	Coordinate Transformation	1
	1.1 Homogeneous Coordinates	1
	1.2 Coordinate Transformation in Matrix Representation	2
	1.3 Rotation About an Axis	6
	1.4 Rotational and Translational $4 \times 4$ Matrices	14
	1.5 Examples of Coordinate Transformation	15
	1.6 Application to Derivation of Curves	24
	1.7 Application to Derivation of Surfaces	28
2	Relative Velocity	33
	2.1 Vector Representation	33
	2.2 Matrix Representation	39
	2.3 Application of Skew-Symmetric Matrices	41
3	Centrodes, Axodes, and Operating Pitch Surfaces	44
	3.1 The Concept of Centrodes	44
	3.2 Pitch Circle	49
	3.3 Operating Pitch Circles	50
	3.4 Axodes in Rotation Between Intersected Axes	51
	3.5 Axodes in Rotation Between Crossed Axes	52
	3.6 Operating Pitch Surfaces for Gears with Crossed Axes	56
4	Planar Curves	59
	4.1 Parametric Representation	59
	4.2 Representation by Implicit Function	60
	4.3 Tangent and Normal to a Planar Curve	60
	4.4 Curvature of Planar Curves	68
5	Surfaces	78
	5.1 Parametric Representation of Surfaces	78
	5.2 Curvilinear Coordinates	78
	5.3 Tangent Plane and Surface Normal	79

vi Contents

	5.4 Representation of a Surface by Implicit Function	82
	5.5 Examples of Surfaces	82
6	Conjugated Surfaces and Curves	97
	6.1 Envelope to a Family of Surfaces: Necessary Condition	
	of Existence	97
	6.2 Basic Kinematic Relations	102
	6.3 Conditions of Nonundercutting	103
	6.4 Sufficient Conditions for Existence of an Envelope	
	to a Family of Surfaces	107
	6.5 Contact Lines; Surface of Action	110
	6.6 Envelope to Family of Contact Lines on Generating	
	Surface $\Sigma_1$	112
	6.7 Formation of Branches of Envelope to Parametric	
	Families of Surfaces and Curves	114
	6.8 Wildhaber's Concept of Limit Contact Normal	118
	6.9 Fillet Generation	119
	6.10 Two-Parameter Enveloping	124
	6.11 Axes of Meshing	128
	6.12 Knots of Meshing	134
	6.13 Problems	137
7	Curvatures of Surfaces and Curves	153
	7.1 Introduction	153
	7.2 Spatial Curve in 3D-Space	153
	7.3 Surface Curves	164
	7.4 First and Second Fundamental Forms	175
	7.5 Principal Directions and Curvatures	180
	7.6 Euler's Equation	188
	7.7 Gaussian Curvature; Three Types of Surface	
	Points	189
	7.8 Dupin's Indicatrix	193
	7.9 Geodesic Line; Surface Torsion	194
8	Mating Surfaces: Curvature Relations, Contact Ellips	<b>e</b> 202
	8.1 Introduction	202
	8.2 Basic Equations	203
	8.3 Planar Gearing: Relation Between Curvatures	204
	8.4 Direct Relations Between Principal Curvatures	
	of Mating Surfaces	218
	8.5 Direct Relations Between Normal Curvatures	
	of Mating Surfaces	226
	8.6 Diagonalization of Curvature Matrix	231
	8.7 Contact Ellipse	234
9	Computerized Simulation of Meshing and Contact	241
	9.1 Introduction	241
	9.2 Predesign of a Parabolic Function of Transmission	
	Errors	242
	9.3 Local Synthesis	245

	9.4 Tooth Contact Analysis	249
	9.5 Application of Finite Element Analysis for Design	
	of Gear Drives	257
	9.6 Edge Contact	260
10	Spur Involute Gears	267
	10.1 Introduction	267
	10.2 Geometry of Involute Curves	268
	10.3 Generation of Involute Curves by Tools	273
	10.4 Tooth Element Proportions	278
	10.5 Meshing of Involute Gear with Rack-Cutter	280
	10.6 Relations Between Tooth Thicknesses Measured	
	on Various Circles	285
	10.7 Meshing of External Involute Gears	287
	10.8 Contact Ratio	292
	10.9 Nonstandard Gears	294
П	Internal Involute Gears	304
	11.1 Introduction	304
	11.2 Generation of Gear Fillet	305
	11.3 Conditions of Nonundercutting	309
	11.4 Interference by Assembly	314
12	Noncircular Gears	318
	12.1 Introduction	318
	12.2 Centrodes of Noncircular Gears	318
	12.3 Closed Centrodes	323
	12.4 Elliptical and Modified Elliptical Gears	326
	12.5 Conditions of Centrode Convexity	329
	12.6 Conjugation of an Eccentric Circular Gear with	
	a Noncircular Gear	330
	12.7 Identical Centrodes	331
	<ul><li>12.8 Design of Combined Noncircular Gear Mechanism</li><li>12.9 Generation Based on Application of Noncircular</li></ul>	333
	Master-Gears	335
	12.10 Enveloping Method for Generation	336
	12.11 Evolute of Tooth Profiles	341
	12.12 Pressure Angle	344
	Appendix 12.A: Displacement Functions for Generation	311
	by Rack-Cutter	345
	Appendix 12.B: Displacement Functions for Generation	3 13
	by Shaper	348
13	Cycloidal Gearing	350
	13.1 Introduction	350
	13.2 Generation of Cycloidal Curves	350
	13.3 Equations of Cycloidal Curves	354
	13.4 Camus' Theorem and Its Application	355
	13.5 External Pin Gearing	359
	13.6 Internal Pin Gearing	365

viii Contents

	13.7 Overcentrode Cycloidal Gearing	367
	13.8 Root's Blower	369
14	Involute Helical Gears with Parallel Axes	375
	14.1 Introduction	375
	14.2 General Considerations	375
	14.3 Screw Involute Surface	377
	14.4 Meshing of a Helical Gear with a Rack	382
	14.5 Meshing of Mating Helical Gears	392
	14.6 Conditions of Nonundercutting	396
	14.7 Contact Ratio	398
	14.8 Force Transmission	399
	14.9 Results of Tooth Contact Analysis (TCA)	402
	14.10 Nomenclature	403
15	Modified Involute Gears	404
13	15.1 Introduction	404
	15.2 Axodes of Helical Gears and Rack-Cutters	407
	15.3 Profile-Crowned Pinion and Gear Tooth Surfaces	411
	15.4 Tooth Contact Analysis (TCA) of Profile-Crowned	711
	Pinion and Gear Tooth Surfaces	414
	15.5 Longitudinal Crowning of Pinion by a Plunging Disk	419
	15.6 Grinding of Double-Crowned Pinion by a Worm	424
	15.7 TCA of Gear Drive with Double-Crowned Pinion	430
	15.8 Undercutting and Pointing	432
	15.9 Stress Analysis	435
16	Involute Helical Gears with Crossed Axes	441
10	16.1 Introduction	441
		443
	<ul><li>16.2 Analysis and Simulation of Meshing of Helical Gears</li><li>16.3 Simulation of Meshing of Crossed Helical Gears</li></ul>	452
	16.4 Generation of Conjugated Tooth Surfaces of Crossed	432
	Helical Gears	455
	16.5 Design of Crossed Helical Gears	458
	16.6 Stress Analysis	465
	Appendix 16.A: Derivation of Shortest Center Distance for	103
	Canonical Design	467
	Appendix 16.B: Derivation of Equation of Canonical Design	707
	$f(\gamma_0, \alpha_{on}, \lambda_{b1}, \lambda_{b2}) = 0$	472
	Appendix 16.C: Relations Between Parameters $\alpha_{pt}$ and $\alpha_{pn}$	473
	Appendix 16.0: Relations between Farameters $\alpha_{pt}$ and $\alpha_{pn}$ Appendix 16.D: Derivation of Equation (16.5.5)	473
	Appendix 16.D. Derivation of Equation (16.5.3)  Appendix 16.E: Derivation of Additional Relations Between	7/3
	$\alpha_{ot1}$ and $\alpha_{ot2}$	474
17	New Version of Novikov–Wildhaber Helical Gears	475
• •	17.1 Introduction	475
	17.1 Introduction 17.2 Axodes of Helical Gears and Rack-Cutter	478
	17.3 Parabolic Rack-Cutters	479
	17.5 Tarabone Rack-Cutters  17.4 Profile-Crowned Pinion and Gear Tooth Surfaces	482

	17.5	Tooth Contact Analysis (TCA) of Gear Drive with	
		Profile-Crowned Pinion	485
	17.6	Longitudinal Crowning of Pinion by a Plunging Disk	487
		Generation of Double-Crowned Pinion by a Worm	491
		TCA of a Gear Drive with a Double-Crowned Pinion	497
	17.9	Undercutting and Pointing	500
		Stress Analysis	502
18	Face.	Gear Drives	508
		Introduction	508
		Axodes, Pitch Surfaces, and Pitch Point	510
		Face-Gear Generation	512
		Localization of Bearing Contact	512
		Equations of Face-Gear Tooth Surface	515
		Conditions of Nonundercutting of Face-Gear Tooth	313
	10.0	Surface (Generated by Involute Shaper)	519
	107	· · · · · · · · · · · · · · · · · · ·	319
	18./	Pointing of Face-Gear Teeth Generated by Involute	522
	10.0	Shaper Fillet Surface	522
			524
		Geometry of Parabolic Rack-Cutters	525
	18.10	Second Version of Geometry: Derivation of Tooth	527
	10 11	Surfaces of Shaper and Pinion	527
	18.11	Second Version of Geometry: Derivation of Face-Gear	520
	10.12	Tooth Surface	529
		Design Recommendations	529
		Tooth Contact Analysis (TCA)	531
		Application of Generating Worm	535
	18.15	Stress Analysis	541
19		m-Gear Drives with Cylindrical Worms	547
		Introduction	547
		Pitch Surfaces and Gear Ratio	548
		Design Parameters and Their Relations	552
		Generation and Geometry of ZA Worms	557
		Generation and Geometry of ZN Worms	561
		Generation and Geometry of ZI (Involute) Worms	574
		Geometry and Generation of K Worms	581
		Geometry and Generation of F-I Worms (Version I)	590
		Geometry and Generation of F-II Worms (Version II)	597
		Generalized Helicoid Equations	601
	19.11	Equation of Meshing of Worm and Worm-Gear	
		Surfaces	603
		Area of Meshing	606
	19.13	Prospects of New Developments	609
20		le-Enveloping Worm-Gear Drives	614
		Introduction	614
		Generation of Worm and Worm-Gear Surfaces	614
		Worm Surface Equations	618
	20.4	Equation of Meshing	620

x Contents

	20.5 Contact Lines	622
	20.6 Worm-Gear Surface Equations	622
21	Spiral Bevel Gears	627
	21.1 Introduction	627
	21.2 Basic Ideas of the Developed Approach	628
	21.3 Derivation of Gear Tooth Surfaces	633
	21.4 Derivation of Pinion Tooth Surface	644
	21.5 Local Synthesis and Determination of Pinion	
	Machine-Tool Settings	649
	21.6 Relationships Between Principal Curvatures and	
	Directions of Mating Surfaces	656
	21.7 Simulation of Meshing and Contact	661
	21.8 Application of Finite Element Analysis for the Design	
	of Spiral Bevel Gear Drives	665
	21.9 Example of Design and Optimization of a Spiral Bevel	
	Gear Drive	666
	21.10 Compensation of the Shift of the Bearing Contact	676
22	Hypoid Gear Drives	679
	22.1 Introduction	679
	22.2 Axodes and Operating Pitch Cones	679
	22.3 Tangency of Hypoid Pitch Cones	680
	22.4 Auxiliary Equations	682
	22.5 Design of Hypoid Pitch Cones	685
	22.6 Generation of Face-Milled Hypoid Gear Drives	690
23	Planetary Gear Trains	697
	23.1 Introduction	697
	23.2 Gear Ratio	697
	23.3 Conditions of Assembly	703
	23.4 Phase Angle of Planet Gears	707
	23.5 Efficiency of a Planetary Gear Train	709
	23.6 Modifications of Gear Tooth Geometry	711
	23.7 Tooth Contact Analysis (TCA)	712
	23.8 Illustration of the Effect of Regulation of Backlash	716
24	Generation of Helicoids	718
	24.1 Introduction	718
	24.2 Generation by Finger-Shaped Tool: Tool Surface is	
	Given	718
	24.3 Generation by Finger-Shaped Tool: Workpiece Surface	
	is Given	723
	24.4 Generation by Disk-Shaped Tool: Tool Surface is Given	726
	24.5 Generation by Disk-Shaped Tool: Workpiece Surface is	
	Given	730
25	Design of Flyblades	734
	25.1 Introduction	734
	25.2 Two-Parameter Form Representation of Worm Surfaces	735

	25.3 Three-Parameter Form Representation of Worm	
	Surfaces	737
	25.4 Working Equations	738
26	Generation of Surfaces by CNC Machines	746
	26.1 Introduction	746
	26.2 Execution of Motions of CNC Machines	747
	26.3 Generation of Hypoid Pinion	750
	26.4 Generation of a Surface with Optimal Approximation	752
27	Overwire (Ball) Measurement	769
	27.1 Introduction	769
	27.2 Problem Description	769
	27.3 Measurement of Involute Worms, Involute Helical	
	Gears, and Spur Gears	773
	27.4 Measurement of Asymmetric Archimedes Screw	779
28	Minimization of Deviations of Gear Real Tooth Surfaces	782
	28.1 Introduction	782
	28.2 Overview of Measurement and Modeling Method	783
	28.3 Equations of Theoretical Tooth Surface $\Sigma_t$	784
	28.4 Coordinate Systems Used for Coordinate	
	Measurements	785
	28.5 Grid and Reference Point	786
	28.6 Deviations of the Real Surface	787
	28.7 Minimization of Deviations	787
Ref	erences	789
Ind	ex	795

## | Coordinate Transformation

### I.I HOMOGENEOUS COORDINATES

A position vector in a three-dimensional space (Fig. 1.1.1) may be represented (i) in vector form as

$$\mathbf{r}_m = \overline{\mathbf{O}_m \mathbf{M}} = x_m \mathbf{i}_m + y_m \mathbf{j}_m + z_m \mathbf{k}_m \tag{1.1.1}$$

where  $(i_m, j_m, k_m)$  are the unit vectors of coordinate axes, and (ii) by the column matrix

$$\mathbf{r}_m = \begin{bmatrix} x_m \\ y_m \\ z_m \end{bmatrix}. \tag{1.1.2}$$

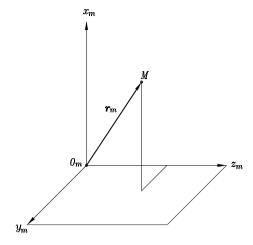
The subscript "m" indicates that the position vector is represented in coordinate system  $S_m(x_m, y_m, z_m)$ . To save space while designating a vector, we will also represent the position vector by the row matrix,

$$\mathbf{r}_m = \begin{bmatrix} x_m & y_m & z_m \end{bmatrix}^{\mathsf{T}}. \tag{1.1.3}$$

The superscript "T" means that  $\mathbf{r}_m^{\mathrm{T}}$  is a transpose matrix with respect to  $\mathbf{r}_m$ .

A point – the end of the position vector – is determined in Cartesian coordinates with three numbers: x, y, z. Generally, coordinate transformation in matrix operations needs mixed matrix operations where both multiplication and addition of matrices must be used. However, only multiplication of matrices is needed if position vectors are represented with homogeneous coordinates. Application of such coordinates for coordinate transformation in theory of mechanisms has been proposed by Denavit & Hartenberg [1955] and by Litvin [1955]. Homogeneous coordinates of a point in a three-dimensional space are determined by four numbers  $(x^*, y^*, z^*, t^*)$  which are not equal to zero simultaneously and of which only three are independent. Assuming that  $t^* \neq 0$ , ordinary coordinates and homogeneous coordinates may be related as follows:

$$x = \frac{x^*}{t^*}$$
  $y = \frac{y^*}{t^*}$   $z = \frac{z^*}{t^*}$ . (1.1.4)



**Figure 1.1.1:** Position vector in Cartesian coordinate system.

With  $t^* = 1$ , a point may be specified by homogeneous coordinates such as (x, y, z, 1), and a position vector may be represented by

$$\mathbf{r}_m = \begin{bmatrix} x_m \\ y_m \\ z_m \\ 1 \end{bmatrix} \text{ or }$$

$$\mathbf{r}_m = [x_m \quad y_m \quad z_m \quad 1]^{\mathrm{T}}.$$

## 1.2 COORDINATE TRANSFORMATION IN MATRIX REPRESENTATION

Consider two coordinate systems  $S_m(x_m, y_m, z_m)$  and  $S_n(x_n, y_n, z_n)$  (Fig. 1.2.1). Point M is represented in coordinate system  $S_m$  by the position vector

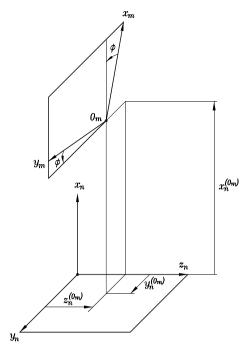
$$\mathbf{r}_m = \begin{bmatrix} x_m & y_m & z_m & 1 \end{bmatrix}^{\mathsf{T}}. \tag{1.2.1}$$

The same point M can be determined in coordinate system  $S_n$  by the position vector

$$\mathbf{r}_n = \begin{bmatrix} x_n & y_n & z_n & 1 \end{bmatrix}^{\mathrm{T}} \tag{1.2.2}$$

with the matrix equation

$$\mathbf{r}_n = \mathbf{M}_{nm} \mathbf{r}_m. \tag{1.2.3}$$



**Figure 1.2.1:** Derivation of coordinate transformation.

Matrix  $M_{nm}$  is represented by

$$\mathbf{M}_{nm} = \begin{bmatrix} a_{11} & a_{12} & a_{13} & a_{14} \\ a_{21} & a_{22} & a_{23} & a_{24} \\ a_{31} & a_{32} & a_{33} & a_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} (\mathbf{i}_{n} \cdot \mathbf{i}_{m}) & (\mathbf{i}_{n} \cdot \mathbf{j}_{m}) & (\mathbf{i}_{n} \cdot \mathbf{k}_{m}) & (\overline{O_{n}O_{m}} \cdot \mathbf{i}_{n}) \\ (\mathbf{j}_{n} \cdot \mathbf{i}_{m}) & (\mathbf{j}_{n} \cdot \mathbf{j}_{m}) & (\mathbf{j}_{n} \cdot \mathbf{k}_{m}) & (\overline{O_{n}O_{m}} \cdot \mathbf{j}_{n}) \\ (\mathbf{k}_{n} \cdot \mathbf{i}_{m}) & (\mathbf{k}_{n} \cdot \mathbf{j}_{m}) & (\mathbf{k}_{n} \cdot \mathbf{k}_{m}) & (\overline{O_{n}O_{m}} \cdot \mathbf{k}_{n}) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} \cos(\widehat{x_{n}}, \widehat{x_{m}}) & \cos(\widehat{x_{n}}, \widehat{y_{m}}) & \cos(\widehat{x_{n}}, \widehat{z_{m}}) & x_{n}^{(O_{m})} \\ \cos(\widehat{y_{n}}, \widehat{x_{m}}) & \cos(\widehat{y_{n}}, \widehat{y_{m}}) & \cos(\widehat{y_{n}}, \widehat{z_{m}}) & y_{n}^{(O_{m})} \\ \cos(\widehat{z_{n}}, \widehat{x_{m}}) & \cos(\widehat{z_{n}}, \widehat{y_{m}}) & \cos(\widehat{z_{n}}, \widehat{z_{m}}) & z_{n}^{(O_{m})} \\ 0 & 0 & 0 & 1 \end{bmatrix}. \tag{1.2.4}$$

Here,  $(i_n, j_n, k_n)$  are the unit vectors of the axes of the "new" coordinate system;  $(i_m, j_m, k_m)$  are the unit vectors of the axes of the "old" coordinate system;  $O_n$  and  $O_m$  are the origins of the "new" and "old" coordinate systems; subscript "nm" in the designation  $M_{nm}$  indicates that the coordinate transformation is performed from  $S_m$  to

 $S_n$ . The determination of elements  $a_{lk}$  (k = 1, 2, 3; l = 1, 2, 3) of matrix  $\mathbf{M}_{nm}$  is based on the following rules:

(i) Elements of the  $3 \times 3$  submatrix

$$\mathbf{L}_{nm} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}$$
 (1.2.5)

represent the direction cosines of the "old" unit vectors  $(\mathbf{i}_m, \mathbf{j}_m, \mathbf{k}_m)$  in the "new" coordinate systems  $S_n$ . For instance,  $a_{21} = \cos(\widehat{y_n}, \widehat{x}_m)$ ,  $a_{32} = \cos(\widehat{z_n}, \widehat{y}_m)$ , and so on. The subscripts of elements  $a_{kl}$  in matrix (1.2.5) indicate the number l of the "old" coordinate axis and the number k of the "new" coordinate axis. Axes x, y, z are given numbers 1, 2, and 3, respectively.

(ii) Elements  $a_{14}$ ,  $a_{24}$ , and  $a_{34}$  represent the "new" coordinates  $x_n^{(O_m)}$ ,  $y_n^{(O_m)}$ ,  $z_n^{(O_m)}$  of the "old" origin  $O_m$ .

Recall that nine elements of matrix  $L_{nm}$  are related by six equations that express the following:

(1) Elements of each row (or column) are direction cosines of a unit vector. Thus,

$$a_{11}^2 + a_{12}^2 + a_{13}^2 = 1,$$
  $a_{11}^2 + a_{21}^2 + a_{31}^2 = 1,$   $\cdots$  (1.2.6)

(2) Due to orthogonality of unit vectors of coordinate axes, we have

$$[a_{11} \ a_{12} \ a_{13}] [a_{21} \ a_{22} \ a_{23}]^{T} = 0$$

$$[a_{11} \ a_{21} \ a_{31}] [a_{12} \ a_{22} \ a_{32}]^{T} = 0.$$
(1.2.7)

An element of matrix  $L_{nm}$  can be represented by a respective determinant of the second order [Strang, 1988]. For instance,

$$a_{11} = \begin{vmatrix} a_{22} & a_{23} \\ a_{32} & a_{33} \end{vmatrix}, \quad a_{23} = (-1) \begin{vmatrix} a_{11} & a_{12} \\ a_{31} & a_{32} \end{vmatrix}.$$
 (1.2.8)

To determine the new coordinates  $(x_n, y_n, z_n, 1)$  of point M, we have to use the rule of multiplication of a square matrix  $(4 \times 4)$  and a column matrix  $(4 \times 1)$ . (The number of rows in the column matrix is equal to the number of columns in matrix  $M_{nm}$ .) Equation (1.2.3) yields

$$x_n = a_{11}x_m + a_{12}y_m + a_{13}z_m + a_{14}$$
  

$$y_n = a_{21}x_m + a_{22}y_m + a_{23}z_m + a_{24}$$
  

$$z_n = a_{31}x_m + a_{32}y_m + a_{33}z_m + a_{34}.$$
(1.2.9)

The purpose of the *inverse* coordinate transformation is to determine the coordinates  $(x_m, y_m, z_m)$ , taking as given coordinates  $(x_n, y_n, z_n)$ . The inverse coordinate transformation is represented by

$$\mathbf{r}_m = \mathbf{M}_{mn} \mathbf{r}_n. \tag{1.2.10}$$

The inverse matrix  $M_{mn}$  indeed exists if the determinant of matrix  $M_{nm}$  differs from zero.

There is a simple rule that allows the elements of the inverse matrix to be determined in terms of elements of the direct matrix. Consider that matrix  $\mathbf{M}_{nm}$  is given by

$$\mathbf{M}_{nm} = \begin{bmatrix} a_{11} & a_{12} & a_{13} & a_{14} \\ a_{21} & a_{22} & a_{23} & a_{24} \\ a_{31} & a_{32} & a_{33} & a_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix}. \tag{1.2.11}$$

It is necessary to determine the elements of matrix  $M_{mn}$  represented by

$$\mathbf{M}_{mn} = \begin{bmatrix} b_{11} & b_{12} & b_{13} & b_{14} \\ b_{21} & b_{22} & b_{23} & b_{24} \\ b_{31} & b_{32} & b_{33} & b_{34} \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$
(1.2.12)

Here,

$$\mathbf{M}_{mn} = \mathbf{M}_{nm}^{-1}, \quad \mathbf{M}_{mn} \mathbf{M}_{nm} = \mathbf{I}$$

where I is the identity matrix.

The submatrix  $L_{mn}$  of the order  $(3 \times 3)$  is determined as follows:

$$\mathbf{L}_{mn} = \begin{bmatrix} b_{11} & b_{12} & b_{13} \\ b_{21} & b_{22} & b_{23} \\ b_{31} & b_{32} & b_{33} \end{bmatrix} = \begin{bmatrix} a_{11} & a_{21} & a_{31} \\ a_{12} & a_{22} & a_{32} \\ a_{13} & a_{23} & a_{33} \end{bmatrix} = \mathbf{L}_{nm}^{\mathsf{T}}.$$
 (1.2.13)

The remaining elements ( $b_{14}$ ,  $b_{24}$ , and  $b_{34}$ ) are determined with the following equations:

$$b_{14} = -(a_{11}a_{14} + a_{21}a_{24} + a_{31}a_{34}) \Rightarrow -\begin{bmatrix} :a_{11}: & a_{12} & a_{13} & :a_{14}: \\ :a_{21}: & a_{22} & a_{23} & :a_{24}: \\ :a_{31}: & a_{32} & a_{33} & :a_{34}: \\ :0: & 0 & 0 & :1: \end{bmatrix}$$

$$b_{24} = -(a_{12}a_{14} + a_{22}a_{24} + a_{32}a_{34}) \Rightarrow -\begin{bmatrix} a_{11} & : a_{12} : & a_{13} & : a_{14} : \\ a_{21} & : a_{22} : & a_{23} & : a_{24} : \\ a_{31} & : a_{32} : & a_{33} & : a_{34} : \\ 0 & : 0 : & 0 & : 1 : \end{bmatrix}$$

$$b_{34} = -(a_{13}a_{14} + a_{23}a_{24} + a_{33}a_{34}) \Rightarrow -\begin{bmatrix} a_{11} & a_{12} & : a_{13} : & : a_{14} : \\ a_{21} & a_{22} & : a_{23} : & : a_{24} : \\ a_{31} & a_{32} & : a_{33} : & : a_{34} : \\ 0 & 0 & : 0 : & : 1 : \end{bmatrix}.$$
(1.2.14)

The columns to be multiplied are marked.

To perform successive coordinate transformation, we need only to follow the product rule of matrix algebra. For instance, the matrix equation

$$\mathbf{r}_{p} = \mathbf{M}_{p(p-1)} \mathbf{M}_{(p-1)(p-2)} \cdots \mathbf{M}_{32} \mathbf{M}_{21} \mathbf{r}_{1}$$
 (1.2.15)

represents successive coordinate transformation from  $S_1$  to  $S_2$ , from  $S_2$  to  $S_3$ , ..., from  $S_{p-1}$  to  $S_p$ .

To perform transformation of components of free vectors, we need only to apply  $3 \times 3$  submatrices L, which may be obtained by eliminating the last row and the last column of the corresponding matrix M. This results from the fact that the free-vector components (projections on coordinate axes) do not depend on the location of the origin of the coordinate system.

The transformation of vector components of a free vector  $\mathbf{A}$  from system  $S_m$  to  $S_n$  is represented by the matrix equation

$$\mathbf{A}_n = \mathbf{L}_{nm} \mathbf{A}_m \tag{1.2.16}$$

where

$$\mathbf{A}_{n} = \begin{bmatrix} A_{xn} \\ A_{yn} \\ A_{zn} \end{bmatrix}, \quad \mathbf{L}_{nm} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}, \quad \mathbf{A}_{m} = \begin{bmatrix} A_{xm} \\ A_{ym} \\ A_{zm} \end{bmatrix}. \quad (1.2.17)$$

A normal to the gear tooth surface is a *sliding* vector because it may be translated along its line of action. However, we may transform the surface normal as a *free* vector if the surface point where the surface normal is considered will be transferred simultaneously.

### 1.3 ROTATION ABOUT AN AXIS

### Two Main Problems

We consider a general case in which the rotation is performed about an axis that does not coincide with any axis of the employed coordinate system. We designate the unit vector of the axis of rotation by c (Fig. 1.3.1) and assume that the rotation about c may be performed either counterclockwise or clockwise.

Henceforth we consider two coordinate systems: (i) the fixed one,  $S_a$ ; and (ii) the movable one,  $S_b$ . There are two typical problems related to rotation about c. The first one can be formulated as follows.

Consider that a position vector is rigidly connected to the movable body. The initial position of the position vector is designated by  $\overline{OA} = \rho$  (Fig. 1.3.1). After rotation through an angle  $\phi$  about c, vector  $\rho$  will take a new position designated by  $\overline{OA}^* = \rho^*$ . Both vectors,  $\rho$  and  $\rho^*$  (Fig. 1.3.1), are considered to be in the *same* coordinate system, say  $S_a$ . Our goal is to develop an equation that relates components of vectors  $\rho_a$  and  $\rho_a^*$ . (The subscript "a" indicates that the two vectors are represented in the *same* coordinate system  $S_a$ .) Matrix equation

$$\rho_a^* = \mathcal{L}_a \rho_a \tag{1.3.1}$$

describes the relation between the components of vectors  $\rho$  and  $\rho^*$  that are represented in the same coordinate system  $S_a$ .

The other problem concerns representation of the *same* position vector in different coordinate systems. Our goal is to derive matrix  $\mathbf{L}_{ba}$  in matrix equation

$$\rho_b = \mathcal{L}_{ba} \rho_a. \tag{1.3.2}$$

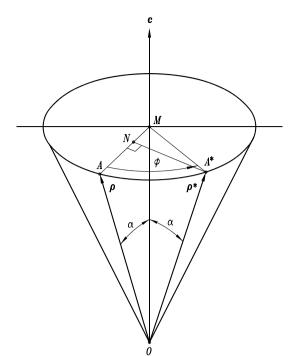


Figure 1.3.1: Rigid body rotation.

The designations  $\rho_a$  and  $\rho_b$  indicate that the *same* position vector  $\rho$  is represented in coordinate systems  $S_a$  and  $S_b$ , respectively. Although the *same* position vector is considered, the components of  $\rho$  in coordinate systems  $S_a$  and  $S_b$  are different and we designate them by

$$\rho_a = a_1 \mathbf{i}_a + a_2 \mathbf{j}_a + a_3 \mathbf{k}_a \tag{1.3.3}$$

and

$$\rho_b = b_1 \mathbf{i}_b + b_2 \mathbf{j}_b + b_3 \mathbf{k}_b. \tag{1.3.4}$$

Matrix  $L_{ba}$  is an operator that transforms the components  $[a_1 \ a_2 \ a_3]^T$  into  $[b_1 \ b_2 \ b_3]^T$ . It will be shown below that operators  $L_a$  and  $L_{ba}$  are related.

**Problem I.** Relations between components of vectors  $\rho_a$  and  $\rho_a^*$ .

Recall that  $\rho_a$  and  $\rho_a^*$  are two position vectors that are represented in the *same* coordinate system  $S_a$ . Vector  $\rho$  represents the initial position of the position vector, *before* rotation, and  $\rho^*$  represents the position vector *after* rotation about c. The following derivations are based on the assumption that rotation about c is performed counterclockwise. The procedure of derivations (see also Suh & Radcliffe, 1978, Shabana, 1989, and others) is as follows.

**Step 1:** We represent  $\rho_a^*$  by the equation (Fig. 1.3.1)

$$\rho_a^* = \overline{OM} + \overline{MN} + \overline{NA^*} \tag{1.3.5}$$

where

$$\overline{OM} = (\mathbf{c}_a \cdot \boldsymbol{\rho}_a)\mathbf{c}_a = (\mathbf{c}_a \cdot \boldsymbol{\rho}_a^*)\mathbf{c}_a \tag{1.3.6}$$

and  $c_a$  is the unit vector of the axis of rotation that is represented in  $S_a$ .

Step 2: Vector  $\rho_a$  is represented by the equation

$$\rho_a = \overline{OM} + \overline{MA} = (\mathbf{c}_a \cdot \boldsymbol{\rho}_a)\mathbf{c}_a + \overline{MA} \tag{1.3.7}$$

that yields

$$\overline{MA} = \rho_a - (\mathbf{c}_a \cdot \rho_a)\mathbf{c}_a. \tag{1.3.8}$$

We emphasize that a vector being rotated about c generates a cone with an apex angle  $\alpha$ . Thus, both vectors,  $\rho$  and  $\rho^*$ , are the generatrices of the same cone, as shown in Fig. 1.3.1.

Step 3: Vector  $\overline{MN}$  has the same direction as  $\overline{MA}$  and this yields

$$|\overline{MN}| = |\overline{MA^*}|\cos\phi = |\overline{MA}|\cos\phi = \rho\sin\alpha\cos\phi \qquad (1.3.9)$$

where  $\alpha$  is the apex angle of the generated cone,  $|\overline{MA}| = \rho \sin \alpha$ , and  $\rho$  is the magnitude of  $\rho$ .

Equations (1.3.8) and (1.3.9) yield

$$\overline{MN} = |\overline{MN}| \frac{\overline{MA}}{|\overline{MA}|} = [\rho_a - (\mathbf{c}_a \cdot \rho_a)\mathbf{c}_a]\cos\phi. \tag{1.3.10}$$

Step 4: Vector  $\overline{NA}^*$  has the same direction as  $(c_a \times \rho_a)$  and may be represented by

$$\overline{NA^*} = \frac{\mathbf{c}_a \times \boldsymbol{\rho}_a}{|\mathbf{c}_a \times \boldsymbol{\rho}_a|} |\overline{NA^*}| = \sin \phi(\mathbf{c}_a \times \boldsymbol{\rho}_a). \tag{1.3.11}$$

Here,

$$|\overline{NA^*}| = |\overline{MA^*}| \sin \phi = \rho \sin \alpha \sin \phi, \quad |\mathbf{c}_a \times \boldsymbol{\rho}_a| = \rho \sin \alpha.$$

Step 5: Equations (1.3.5), (1.3.6), (1.3.10), and (1.3.11) yield

$$\rho_a^* = \rho_a \cos \phi + (1 - \cos \phi)(\mathbf{c}_a \cdot \rho_a)\mathbf{c}_a + \sin \phi(\mathbf{c}_a \times \rho_a). \tag{1.3.12}$$

Step 6: It is easy to prove that

$$(\mathbf{c}_a \cdot \boldsymbol{\rho}_a)\mathbf{c}_a = \mathbf{c}_a \times (\mathbf{c}_a \times \boldsymbol{\rho}_a) + \boldsymbol{\rho}_a \tag{1.3.13}$$

because

$$\mathbf{c}_a \times (\mathbf{c}_a \times \boldsymbol{\rho}_a) = (\mathbf{c}_a \cdot \boldsymbol{\rho}_a)\mathbf{c}_a - \boldsymbol{\rho}_a(\mathbf{c}_a \cdot \mathbf{c}_a).$$

**Step 7:** Equations (1.3.12) and (1.3.13) yield

$$\rho_a^* = \rho_a + (1 - \cos\phi)[\mathbf{c}_a \times (\mathbf{c}_a \times \boldsymbol{\rho}_a)] + \sin\phi(\mathbf{c}_a \times \boldsymbol{\rho}_a). \tag{1.3.14}$$

Equation (1.3.14) is known as the Rodrigues formula. According to the investigation by Cheng & Gupta [1989], this equation deserves to be called the Euler–Rodrigues, formula.

**Step 8:** Additional derivations are directed at representation of the Euler–Rodrigues formula in matrix form.

The cross product  $(c_a \times \rho_a)$  may be represented in matrix form by

$$\mathbf{c}_a \times \boldsymbol{\rho}_a = \mathbf{C}^s \boldsymbol{\rho}_a \tag{1.3.15}$$

where C<sup>s</sup> is the skew-symmetric matrix represented by

$$\mathbf{C}^{s} = \begin{bmatrix} 0 & -c_{3} & c_{2} \\ c_{3} & 0 & -c_{1} \\ -c_{2} & c_{1} & 0 \end{bmatrix}. \tag{1.3.16}$$

Vector  $\mathbf{c}_a$  is represented by

$$\mathbf{c}_a = c_1 \mathbf{i}_a + c_2 \mathbf{j}_a + c_3 \mathbf{k}_a. \tag{1.3.17}$$

**Step 9:** Equations (1.3.14), (1.3.15), and (1.3.16) yield the following matrix representation of the Euler–Rodrigues formula:

$$\rho_a^* = \left[ I + (1 - \cos \phi)(C^s)^2 + \sin \phi C^s \right] \rho_a = L_a \rho_a$$
 (1.3.18)

where I is the  $3 \times 3$  identity matrix. While deriving Eqs. (1.3.14) and (1.3.18), we assumed that the rotation is performed counterclockwise. For the case of clockwise rotation, it is necessary to change the sign preceding  $\sin \phi$  to its opposite. The expression for matrix  $L_a$  that will cover two directions of rotation is

$$L_a = I + (1 - \cos \phi)(C^s)^2 \pm \sin \phi C^s.$$
 (1.3.19)

The upper sign preceding  $\sin \phi$  corresponds to counterclockwise rotation and the lower sign corresponds to rotation in a clockwise direction. In both cases the unit vector **c** must be expressed by the same Eq. (1.3.17) that determines the orientation of **c** but not the direction of rotation. The direction of rotation is identified with the proper sign preceding  $\sin \phi$  in Eq. (1.3.19).

**Problem 2.** Recall that our goal is to derive the operator  $L_{ba}$  in matrix equation (1.3.2) that transforms components of the *same* vector (see Eqs. (1.3.3) and (1.3.4)). It will be shown below that the sought-for operator is represented as

$$\mathbf{L}_{ba} = \mathbf{L}_{a}^{\mathrm{T}} = \mathbf{I} + (1 - \cos\phi)(\mathbf{C}^{s})^{2} \mp \sin\phi\mathbf{C}^{s}. \tag{1.3.20}$$

Operator  $L_{ba}$  can be obtained from operator  $L_a$  given by Eq. (1.3.19) by changing the sign of the angle of rotation,  $\phi$ . The upper and lower signs preceding  $\sin \phi$  in Eq. (1.3.20) correspond to the cases where  $S_a$  will coincide with  $S_b$  by rotation counterclockwise and clockwise, respectively. The proof is based on the determination of components of the same vector, say vector  $\overline{OA}$  shown in Fig. 1.3.1, in coordinate systems  $S_a$  and  $S_b$ .

Step 1: We consider initially that vector  $\overline{OA}$  is represented in  $S_a$  as

$$\rho_a = [a_1 \ a_2 \ a_3]^{\mathrm{T}}. \tag{1.3.21}$$

**Step 2:** To determine components of vector  $\overline{OA}$  in  $S_b$  we consider first that coordinate system  $S_b$  and the previously mentioned position vector are rotated as one rigid body

about c. After rotation through angle  $\phi$ , position vector  $\overline{OA}$  will take the position  $\overline{OA}^*$  and can be represented in  $S_b$  as

$$\overline{OA}^* = a_1 \mathbf{i}_b + a_2 \mathbf{j}_b + a_3 \mathbf{k}_b.$$
 (1.3.22)

It is obvious that vector  $\overline{OA}^*$  has in  $S_b$  the same components as vector  $\overline{OA}$  has in  $S_a$ .

Step 3: We consider now in  $S_b$  two vectors  $\overline{OA}^*$  and  $\overline{OA}$ . Vector  $\overline{OA}^*$  will coincide with  $\overline{OA}$  after clockwise rotation about c. The components of vectors  $\overline{OA}^*$  and  $\overline{OA}$  in  $S_b$  are related by an equation that is similar to Eq. (1.3.19). The difference is that we now have to consider that the rotation from  $\overline{OA}^*$  to  $\overline{OA}$  is performed clockwise. Then we obtain

$$(\overline{OA})_b = \mathcal{L}_b(\overline{OA}^*)_b = \left[\mathbf{I} + (1 - \cos\phi)(\mathbf{C}^s)^2 - \sin\phi\mathbf{C}^s\right](\overline{OA}^*)_b. \tag{1.3.23}$$

Designating components of  $(\overline{OA})_b$  by  $[b_1 \ b_2 \ b_3]^T$ , we receive

$$[b_1 \ b_2 \ b_3]^{\mathrm{T}} = [\mathbf{I} + (1 - \cos \phi)(\mathbf{C}^s)^2 - \sin \phi \mathbf{C}^s][a_1 \ a_2 \ a_3]^{\mathrm{T}}. \tag{1.3.24}$$

**Step 4:** We have now obtained components of the same vector  $\overline{OA}$  in coordinate systems  $S_a$  and  $S_b$ , respectively. The matrix equation that describes transformation of components of  $\overline{OA}$  is

$$(\overline{OA})_b = \mathcal{L}_{ba}(\overline{OA})_a. \tag{1.3.25}$$

For the case in which rotation from  $S_a$  to  $S_b$  is performed counterclockwise we have obtained that

$$\mathbf{L}_{ba} = \mathbf{I} + (1 - \cos \phi)(\mathbf{C}^{s})^{2} - \sin \phi \mathbf{C}^{s}. \tag{1.3.26}$$

Similarly, for the case in which rotation from  $S_a$  to  $S_b$  is performed clockwise, we obtain

$$\mathbf{L}_{ba} = \mathbf{I} + (1 - \cos \phi)(\mathbf{C}^{s})^{2} + \sin \phi \mathbf{C}^{s}. \tag{1.3.27}$$

The general description of operator  $L_{ba}$  and the respective coordinate transformation are as follows:

$$\rho_b = \mathcal{L}_{ba} \rho_a = \left[ \mathbf{I} + (1 - \cos \phi)(\mathbf{C}^s)^2 \mp \sin \phi \mathbf{C}^s \right] \rho_a. \tag{1.3.28}$$

The upper and lower signs preceding  $\sin \phi$  correspond to the cases in which rotation from  $S_a$  to  $S_b$  is performed counterclockwise and clockwise, respectively.

In our identification of coordinate systems  $S_a$  and  $S_b$  we do not use the terms fixed and movable. We just consider that  $S_a$  is the previous coordinate system and  $S_b$  is the new one, and we take into account how the rotation from  $S_a$  to  $S_b$  is performed: counterclockwise or clockwise.

### Matrix Lba

Using Eqs. (1.3.26) and (1.3.27), we may represent elements of matrix  $L_{ba}$  in terms of components of unit vector  $\mathbf{c}$  of the axis of rotation and the angle of rotation  $\phi$ . Thus,

 $y_a$   $y_b$   $z_a, z_b$ 

**Figure 1.3.2:** Derivation of coordinate transformation by rotation.

we obtain

$$\mathbf{L}_{ba} = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}. \tag{1.3.29}$$

Here,

$$a_{11} = \cos\phi \left(1 - c_1^2\right) + c_1^2$$

$$a_{12} = (1 - \cos\phi)c_1c_2 \pm \sin\phi c_3$$

$$a_{13} = (1 - \cos\phi)c_1c_3 \mp \sin\phi c_2$$

$$a_{21} = (1 - \cos\phi)c_1c_2 \mp \sin\phi c_3$$

$$a_{22} = \cos\phi \left(1 - c_2^2\right) + c_2^2$$

$$a_{23} = (1 - \cos\phi)c_2c_3 \pm \sin\phi c_1$$

$$a_{31} = (1 - \cos\phi)c_1c_3 \pm \sin\phi c_2$$

$$a_{32} = (1 - \cos\phi)c_2c_3 \mp \sin\phi c_1$$

$$a_{33} = \cos\phi \left(1 - c_3^2\right) + c_3^2.$$
(1.3.30)

When the axis of rotation coincides with a coordinate axis of  $S_a$ , we have to make two components of unit vector  $\mathbf{c}_a$  equal to zero in Eqs. (1.3.30). For instance, in the case in which rotation is performed about the  $z_a$  axis (Fig. 1.3.2), we have

$$\mathbf{c}_a = \mathbf{k}_a = [0 \ 0 \ 1]^{\mathrm{T}}.$$
 (1.3.31)

We emphasize again that in all cases of coordinate transformation only elements (1.3.30) of matrix  $L_{ba}$ , and not the components of  $c_a$ , depend on the direction of rotation. The unit vector c can be represented in either of the two coordinate systems,  $S_a$  and  $S_b$ , by the equations

$$\mathbf{c} = c_1 \mathbf{i}_a + c_2 \mathbf{j}_a + c_3 \mathbf{k}_a = c_1 \mathbf{i}_b + c_2 \mathbf{j}_b + c_3 \mathbf{k}_b. \tag{1.3.32}$$

This means that the unit vector  $\mathbf{c}$  of the axis of rotation has the *same* components in both coordinate systems,  $S_a$  and  $S_b$ . It is easily verified that

$$[c_1 \ c_2 \ c_3]^{\mathsf{T}} = \mathbf{L}_{ba}[c_1 \ c_2 \ c_3]^{\mathsf{T}}.$$
 (1.3.33)